

## FSBM15SL60

## **SPM™** (Smart Power Module)

### **General Description**

FSBM15SL60 is an advanced smart power module (SPM) that Fairchild has newly developed and designed to provide very compact and low cost, yet high performance ac motor drives mainly targeting low speed low-power inverter-driven application like air conditioners. It combines optimized circuit protection and drive matched to low-loss IGBTs. Highly effective short-circuit current detection/protection is realized through the use of advanced current sensing IGBT chips that allow continuous monitoring of the IGBTs current. System reliability is further enhanced by the integrated under-voltage lock-out protection. The high speed built-in HVIC provides opto-coupler-less IGBT gate driving capability that further reduce the overall size of the inverter system design. In addition the incorporated HVIC facilitates the use of single-supply drive topology enabling the FSBM15SL60 to be driven by only one drive supply voltage without negative bias. Inverter current sensing application can be achieved due to the divided negative dc terminals.

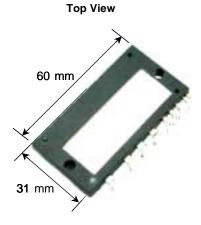
### **Features**

- UL Certified No. E209204
- 600V-15A 3-phase IGBT inverter bridge including control ICs for gate driving and protection
- Divided negative dc-link terminals for inverter current sensing applications
- Single-grounded power supply due to built-in HVIC
- · Typical switching frequency of 3kHz
- Inverter power rating of 1kW / 100~253 Vac
- Isolation rating of 2500Vrms/min.
- Very low leakage current due to using ceramic substrate
- Adjustable current protection level by varying series resistor value with sense-IGBTs

### **Applications**

- AC 100V ~ 253V three-phase inverter drive for small power (1kW) ac motor drives
- Home appliances applications requiring low switching frequency operation like air conditioners drive system
- · Application ratings:
  - Power : 1kW / 100~253 Vac
  - Switching frequency: Typical 15kHz (PWM Control)
  - 100% load current : 7.0A (Irms)

### **External View**



### **Bottom View**



Fig. 1.

## **Integrated Power Functions**

• 600V-15A IGBT inverter for three-phase DC/AC power conversion (Please refer to Fig. 3)

## **Integrated Drive, Protection and System Control Functions**

- For inverter high-side IGBTs: Gate drive circuit, High voltage isolated high-speed level shifting Control circuit under-voltage (UV) protection
  - Note) Available bootstrap circuit example is given in Figs. 10, 15and 16.
- For inverter low-side IGBTs: Gate drive circuit, Short circuit protection (SC)
   Control supply circuit under-voltage (UV) protection
- Fault signaling: Corresponding to a SC fault (Low-side IGBTs) or a UV fault (Low-side supply)
- Input interface: 5V CMOS/LSTTL compatible, Schmitt trigger input

## **Pin Configuration**

### **Top View**

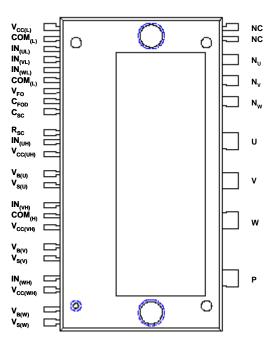


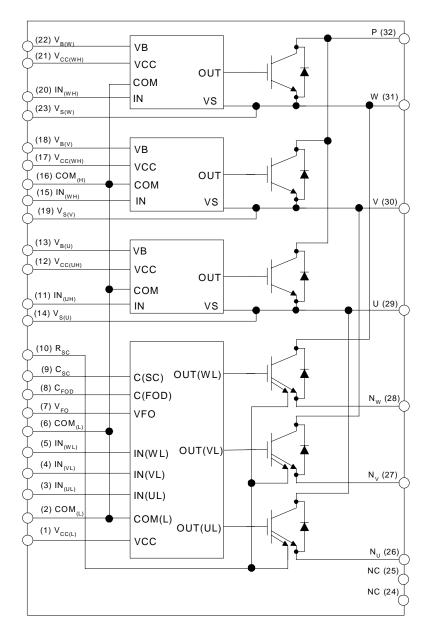
Fig. 2.

# **Pin Descriptions**

Pin Number	Pin Name	Pin Description	
1	$V_{CC(L)}$	Low-side Common Bias Voltage for IC and IGBTs Driving	
2	COM <sub>(L)</sub>	Low-side Common Supply Ground	
3	IN <sub>(UL)</sub>	Signal Input Terminal for Low-side U Phase	
4	IN <sub>(VL)</sub>	Signal Input Terminal for Low-side V Phase	
5	IN <sub>(WL)</sub>	Signal Input Terminal for Low-side W Phase	
6	COM <sub>(L)</sub>	Low-side Common Supply Ground	
7	$V_{FO}$	Fault Output Terminal	
8	$C_FOD$	Capacitor for Fault Output Duration Time Selection	
9	C <sub>SC</sub>	Capacitor (Low-pass Filter) for Short-current Detection Input	
10	R <sub>SC</sub>	Resistor for Short-circuit Current Detection	
11	IN <sub>(UH)</sub>	Signal Input Terminal for High-side U Phase	
12	V <sub>CC(UH)</sub>	High-side Bias Voltage for U Phase IC	
13	V <sub>B(U)</sub>	High-side Bias Voltage for U Phase IGBT Driving	
14	V <sub>S(U)</sub>	High-side Bias Voltage Ground for U Phase IGBT Driving	
15	IN <sub>(VH)</sub>	Signal Input Terminal for High-side V Phase	
16	COM <sub>(H)</sub>	High-side Common Supply Ground	
17	V <sub>CC(VH)</sub>	High-side Bias Voltage for V Phase IC	
18	$V_{B(V)}$	High-side Bias Voltage for V Phase IGBT Driving	
19	$V_{S(V)}$	High-side Bias Voltage Ground for V Phase IGBT Driving	
20	IN <sub>(WH)</sub>	Signal Input Terminal for High-side W Phase	
21	V <sub>CC(WH)</sub>	High-side Bias Voltage for W Phase IC	
22	$V_{B(W)}$	High-side Bias Voltage for W Phase IGBT Driving	
23	V <sub>S(W)</sub>	High-side Bias Voltage Ground for W Phase IGBT Driving	
24	NC	No Connection	
25	NC	No Connection	
26	N <sub>U</sub>	Negative DC-Link Input Terminal for U Phase	
27	$N_V$	Negative DC-Link Input Terminal for V Phase	
28	N <sub>W</sub>	Negative DC-Link Input Terminal for W Phase	
29	U	Output Terminal for U Phase	
30	V	Output Terminal for V Phase	
31	W	Output Terminal for W Phase	
32	Р	Positive DC-Link Input Terminal	

## **Internal Equivalent Circuit and Input/Output Pins**

### **Bottom View**



- 1. Inverter low-side is composed of three sense-IGBTs including freewheeling diodes for each IGBT and one control IC which has gate driving, current sensing and protection functions.

  2. Inverter power side is composed of three normal-IGBTs including freewheeling diodes and three drive ICs for each IGBT.

Fig. 3.

# **Absolute Maximum Ratings**

Inverter Part (T<sub>C</sub> = 25°C, Unless Otherwise Specified)

Item	Symbol	Condition	Rating	Unit
Supply Voltage	$V_{DC}$	Applied to DC - Link	450	V
Supply Voltage (Surge)	V <sub>PN(Surge)</sub>	Applied between P- N	500	V
Collector-emitter Voltage	V <sub>CES</sub>		600	V
Each IGBT Collector Current	± I <sub>C</sub>	T <sub>C</sub> = 25°C	15	Α
Each IGBT Collector Current	± I <sub>C</sub>	T <sub>C</sub> = 100°C	10	Α
Each IGBT Collector Current (Peak)	± I <sub>CP</sub>	T <sub>C</sub> = 25°C	30	Α
Collector Dissipation	P <sub>C</sub>	T <sub>C</sub> = 25°C per One Chip	46	W
Operating Junction Temperature	TJ	(Note 1)	-55 ~ 150	°C

Note:

1. It would be recommended that the average junction temperature should be limited to  $T_J \le 125^{\circ}C$  (@ $T_C \le 100^{\circ}C$ ) in order to guarantee safe operation.

## Control Part (T<sub>C</sub> = 25°C, Unless Otherwise Specified)

Item	Symbol	Condition	Rating	Unit
Control Supply Voltage	V <sub>CC</sub>	Applied between V <sub>CC(H)</sub> - COM <sub>(H)</sub> , V <sub>CC(L)</sub> - COM <sub>(L)</sub>	18	V
High-side Control Bias Voltage	V <sub>BS</sub>	Applied between $V_{B(U)}$ - $V_{S(U)}$ , $V_{B(V)}$ - $V_{S(V)}$ , $V_{B(W)}$ - $V_{S(W)}$	20	V
Input Signal Voltage	V <sub>IN</sub>	Applied between $IN_{(UH)}$ , $IN_{(VH)}$ , $IN_{(WH)}$ - $COM_{(H)}$ $IN_{(UL)}$ , $IN_{(VL)}$ , $IN_{(WL)}$ - $COM_{(L)}$	-0.3 ~ 6.0	V
Fault Output Supply Voltage	$V_{FO}$	Applied between V <sub>FO</sub> - COM <sub>(L)</sub>	-0.3~V <sub>CC</sub> +0.5	V
Fault Output Current	I <sub>FO</sub>	Sink Current at V <sub>FO</sub> Pin	5	mA
Current Sensing Input Voltage	$V_{SC}$	Applied between C <sub>SC</sub> - COM <sub>(L)</sub>	-0.3~V <sub>CC</sub> +0.5	V

## **Total System**

Item	Symbol	Condition	Rating	Unit
Self Protection Supply Voltage Limit (Short Circuit Protection Capability)	V <sub>PN(PROT)</sub>	Applied to DC - Link, $V_{CC} = V_{BS} = 13.5 \sim 16.5V$ $T_{J} = 125^{\circ}C$ , Non-repetitive, less than 6 $\mu$ s	400	V
Module Case Operation Temperature	T <sub>C</sub>	Note Fig.4	-20 ~ 100	°C
Storage Temperature	T <sub>STG</sub>		-50 ~ 150	°C
Isolation Voltage	V <sub>ISO</sub>	60Hz, Sinusoidal, AC 1 minute, Connection Pins to Heat-sink Plate	2500	V <sub>rms</sub>

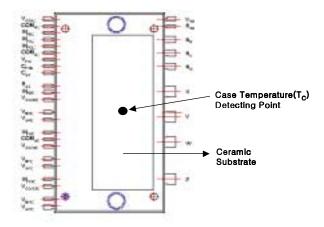


Fig. 4. T<sub>C</sub> Measurement Point

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# **Absolute Maximum Ratings**

## **Thermal Resistance**

Item	Symbol	Condition	Min.	Тур.	Max.	Unit
Junction to Case Thermal Resistance	R <sub>th(j-c)Q</sub>	Each IGBT under Inverter Operating Condition		1	2.71	°C/W
	R <sub>th(j-c)F</sub>	Each FWDi under Inverter Operating Condition	-	1	3.71	°C/W
Contact Thermal Resistance	R <sub>th(c-f)</sub>	Ceramic Substrate (per 1 Module) Thermal Grease Applied	-	1	0.06	°C/W

 $\label{eq:Note:2} \textbf{Note:} \\ 2. \ \ \text{For the measurement point of case temperature}(T_C), \ \text{please refr to Fig. 4}.$ 

### **Electrical Characteristics**

Inverter Part (T<sub>j</sub> = 25°C, Unless Otherwise Specified)

Item	Symbol	Conditi	on	Min.	Тур.	Max.	Unit
Collector - emitter	V <sub>CE(SAT)</sub>	$V_{CC} = V_{BS} = 15V$ $V_{IN} = 0V$	$I_C = 15A, T_j = 25^{\circ}C$	-	-	2.3	V
Saturation Voltage	, ,	$V_{IN} = 0V$	$I_C = 15A, T_i = 125^{\circ}C$	-	-	2.4	V
FWDi Forward Voltage	$V_{FM}$	V <sub>IN</sub> = 5V	I <sub>C</sub> = 15A, T <sub>i</sub> = 25°C	-	-	2.5	V
			$I_C = 15A, T_j = 125^{\circ}C$	-	-	2.3	V
Switching Times	t <sub>ON</sub>		$V_{PN} = 300V, V_{CC} = V_{BS} = 15V$			-	us
	t <sub>C(ON)</sub>	$I_C = 15A, T_j = 25^{\circ}C$		-	0.12	-	us
	t <sub>OFF</sub>	$V_{IN} = 5V \leftrightarrow 0V$ , Inductive Lot (High-Low Side)	oad	-	1.0	-	us
	t <sub>C(OFF)</sub>	(Figit-Low Side)		-	0.6	-	us
	t <sub>rr</sub>	(Note 3)		-	0.1	-	us
Collector - emitter Leakage Current	I <sub>CES</sub>	$V_{CE} = V_{CES}, T_j = 25^{\circ}C$		-	-	250	uA

Note:

3. to<sub>N</sub> and to<sub>FF</sub> include the propagation delay time of the internal drive IC. t<sub>C(ON)</sub> and t<sub>C(OFF)</sub> are the switching time of IGBT itself under the given gate driving condition internally. For the detailed information, please see Fig. 5.

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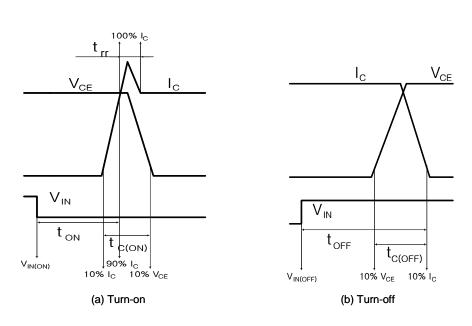


Fig. 5. Switching Time Definition

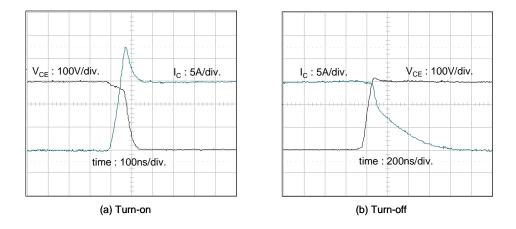


Fig. 6. Experimental Results of Switching Waveforms Test Condition: Vdc=300V, Vcc=15V, L=500uH (Inductive Load),  $T_C$ =25°C

## **Electrical Characteristics**

Control Part (T<sub>i</sub> = 25°C, Unless Otherwise Specified)

Item	Symbol		Condition	Min.	Тур.	Max.	Unit
Control Supply Voltage	V <sub>CC</sub>	Applied between V <sub>CC</sub>	<sub>(H)</sub> ,V <sub>CC(L)</sub> - COM	13.5	15	16.5	V
High-side Bias Voltage	$V_{BS}$	Applied between V <sub>B(U</sub>	) - V <sub>S(U)</sub> , V <sub>B(V)</sub> - V <sub>S(V)</sub> ,	13.5	15	16.5	V
		V <sub>B(W)</sub> - V <sub>S(W)</sub>					
Quiescent V <sub>CC</sub> Supply Cur-	IQCCL	V <sub>CC</sub> = 15V	V <sub>CC(L)</sub> - COM <sub>(L)</sub>	-	-	26	mA
rent		$IN_{(UL, VL, WL)} = 5V$					
	I <sub>QCCH</sub>	V <sub>CC</sub> = 15V	$V_{CC(U)}, V_{CC(V)}, V_{CC(W)} - COM_{(H)}$	-	-	130	uA
Ovices ant V Supply Cur	1	IN <sub>(UH, VH, WH)</sub> = 5V	\ \ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\			420	uA
Quiescent V <sub>BS</sub> Supply Cur- rent	I <sub>QBS</sub>	V <sub>BS</sub> = 15V	V <sub>B(U)</sub> - V <sub>S(U)</sub> , V <sub>B(V)</sub> -V <sub>S(V)</sub> ,	-	-	420	uA
Fault Output Voltage	V	$IN_{(UH, VH, WH)} = 5V$ $V_{SC} = 0V, V_{FO}$ Circuit:	V <sub>B(W)</sub> - V <sub>S(W)</sub>	4.5	-	_	V
radit Odtput Voltage	V <sub>FOH</sub>						V
	V <sub>FOL</sub>	V <sub>SC</sub> = 1V, V <sub>FO</sub> Circuit		-	-	1.1	
PWM Input Frequency	f <sub>PWM</sub>	$T_C \le 100^{\circ}C, T_J \le 125^{\circ}$	<sup>3</sup> C	-	3	-	kHz
Allowable Input Signal	t <sub>dead</sub>	-20°C ≤ T <sub>C</sub> ≤ 100°C		3	-	-	us
Blanking Time considering Leg Arm-short							
Short Circuit Trip Level	\/	T - 25°C \/ - 15\/	(Note 4)	0.45	0.51	0.56	V
<del></del>	V <sub>SC(ref)</sub>	$T_J = 25^{\circ}C, V_{CC} = 15V$					
Sensing Voltage of IGBT Current	V <sub>SEN</sub>	$ -20^{\circ}C \le I_C \le 100^{\circ}C$ , (N) = 0 Ω and $I_C = 15A$ (N)	$Ω R_{SC} = 82 Ω, R_{SU} = R_{SV} = R_{SW}$	0.37	0.45	0.56	V
	111/		1	44.5	40	40.5	V
Supply Circuit Under-	UV <sub>CCD</sub>	T <sub>J</sub> ≤ 125°C	Detection Level	11.5	12	12.5	
Voltage Protection	UV <sub>CCR</sub>		Reset Level	12	12.5	13	V
	UV <sub>BSD</sub>		Detection Level	7.3	9.0	10.8	V
	UV <sub>BSR</sub>		Reset Level	8.6	10.3	12	V
Fault-out Pulse Width	t <sub>FOD</sub>	$C_{FOD} = 33nF \text{ (Note 5)}$	1	1.4	1.8	2.0	ms
ON Threshold Voltage	V <sub>IN(ON)</sub>	High-Side	Applied between IN <sub>(UH)</sub> , IN <sub>(VH)</sub> ,	-	-	0.8	V
OFF Threshold Voltage	V <sub>IN(OFF)</sub>	1	IN <sub>(WH)</sub> - COM <sub>(H)</sub>	3.0	-	-	V
ON Threshold Voltage	V <sub>IN(ON)</sub>	Low-Side	Applied between IN <sub>(UL)</sub> , IN <sub>(VL)</sub> ,	-	-	8.0	V
OFF Threshold Voltage	V <sub>IN(OFF)</sub>		IN <sub>(WL)</sub> - COM <sub>(L)</sub>	3.0	-	-	V

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<sup>Note:
4. Short-circuit current protection is functioning only at the low-sides. It would be recommended that the value of the external sensing resistor (R<sub>SC</sub>) should be selected around 56 Ω in order to make the SC trip-level of about 22A at the shunt resistors (R<sub>SU</sub>,R<sub>SV</sub>,R<sub>SW</sub>) of 0Ω. For the detailed information about the relationship between the external sensing resistor (R<sub>SC</sub>) and the shunt resistors (R<sub>SU</sub>,R<sub>SV</sub>,R<sub>SW</sub>), please see Fig. 7.
5. The fault-out pulse width t<sub>FOD</sub> depends on the capacitance value of C<sub>FOD</sub> according to the following approximate equation: C<sub>FOD</sub> = 18.3 x 10<sup>-6</sup> x t<sub>FOD</sub>[F]</sup> 

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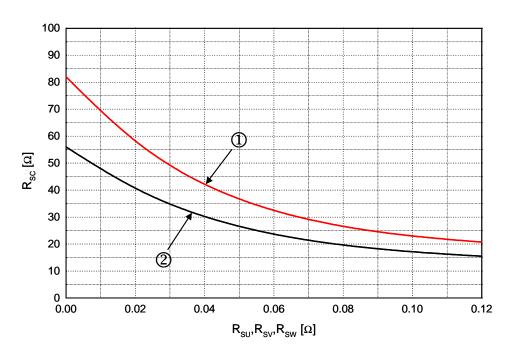


Fig. 7. R<sub>SC</sub> Variation by change of Shunt Resistors (R<sub>SU</sub>, R<sub>SV</sub>, R<sub>SW</sub>) for Short-Circuit Protection ① @ around 100% Rated Current Trip (I<sub>C</sub> '=. 15A) ② @ around 150% Rated Current Trip (I<sub>C</sub> '=. 22A)

# **Mechanical Characteristics and Ratings**

ltam.		· andition	Limits			Linita	
Item		Condition	Min.	Тур.	Max.	Units	
Mounting Torque	Mounting Screw: M4	Recommended 10Kg•cm	8	10	12	Kg•cm	
	(Note 6 and 7)	Recommended 0.98N•m	0.78	0.98	1.17	N•m	
Ceramic Flatness		Note Fig.8	0	-	+120	um	
Weight			-	35	-	g	

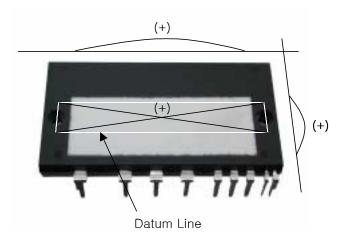


Fig. 8. Flatness Measurement Position of The Ceramic Substrate

- 6. Do not make over torque or mounting screws. Much mounting torque may cause ceramic cracks and bolts and Al heat-fin destruction.

  7. Avoid one side tightening stress. Fig.9 shows the recommended torque order for mounting screws. Uneven mounting can cause the SPM ceramic substrate to be damaged.

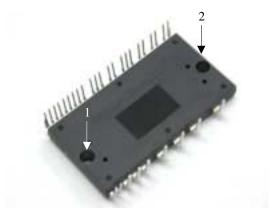
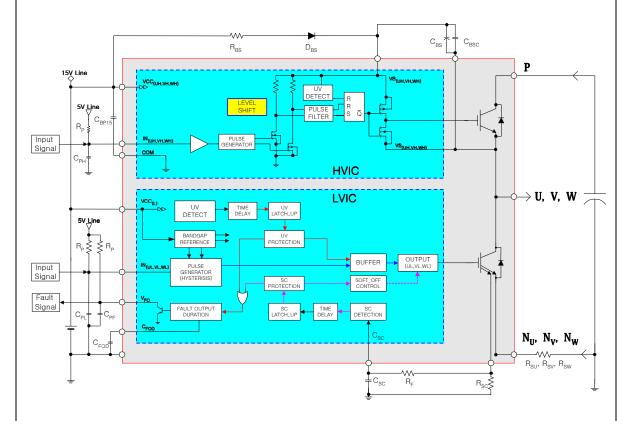


Fig. 9. Mounting Screws Torque Order (1  $\rightarrow$  2)

## **Recommended Operating Conditions**

Itama	Cumbal	Symbol Condition -		Value		
Item	Symbol			Тур.	Max.	Unit
Supply Voltage	$V_{PN}$	Applied between P - N	-	300	400	V
Control Supply Voltage	V <sub>CC</sub>	Applied between V <sub>CC(H)</sub> - COM, V <sub>CC(L)</sub> - COM	13.5	15	16.5	V
High-side Bias Voltage	V <sub>BS</sub>	Applied between $V_{B(U)}$ - $V_{S(U)}$ , $V_{B(V)}$ - $V_{S(V)}$ , $V_{B(W)}$ - $V_{S(W)}$	13.5	15	16.5	V
Blanking Time for Preventing Arm-short	t <sub>dead</sub>	For Each Input Signal	3	-	-	us
PWM Input Signal	f <sub>PWM</sub>	T <sub>C</sub> ≤ 100°C, T <sub>J</sub> ≤ 125°C	-	3	-	kHz
Input ON Threshold Voltage	V <sub>IN(ON)</sub>	Applied between U <sub>IN</sub> ,V <sub>IN</sub> , W <sub>IN</sub> - COM		0 ~ 0.65	5	V
Input OFF Threshold Voltage	V <sub>IN(OFF)</sub>	Applied between U <sub>IN</sub> ,V <sub>IN</sub> , W <sub>IN</sub> - COM		4 ~ 5.5		V

## **ICs Internal Structure and Input/Output Conditions**

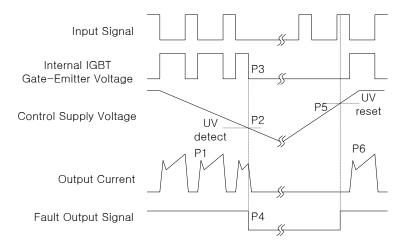


- 1. One LVIC drives three Sense-IGBTs and can do short-circuit current protection also. Three sense emitters are commonly connected to RSC terminal to detect
- short-circuit current. Low-side part of the inverter consists of three sense-IGBTs
  One HVIC drives one normal-IGBT. High-side part of the inverter consists of three normal-IGBTs

- 3. Each IC has under voltage detection and protection function.
  4. The logic input is compatible with standard CMOS or LSTTL outputs.
  5. R<sub>PCP</sub> coupling at each input/output is recommended in order to prevent the gating input/output signals oscillation and it should be as close as possible to each
- 6. It would be recommended that the bootstrap diode, D<sub>BS</sub>, has soft and fast recovery characteristics.

Fig. 10.

## **Time Charts of SPMs Protective Function**

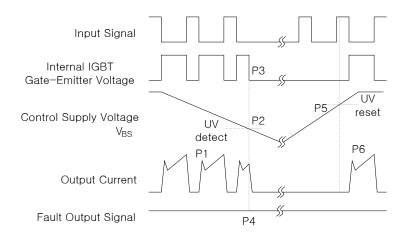


P1: Normal operation - IGBT ON and conducting current

P2 : Under voltage detection P3 : IGBT gate interrupt P4 : Fault signal generation P5 : Under voltage reset

P6: Normal operation - IGBT ON and conducting current

Fig. 11. Under-Voltage Protection (Low-side)



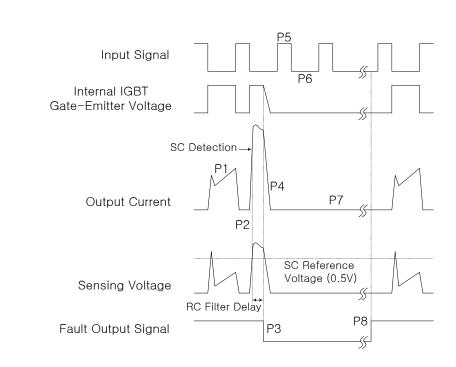
P1: Normal operation - IGBT ON and conducting current

P2 : Under voltage detection P3 : IGBT gate interrupt P4 : No fault signal P5 : Under voltage reset

P6 : Normal operation - IGBT ON and conducting current

Fig. 12. Under-Voltage Protection (High-side)

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P1: Normal operation - IGBT ON and conducting currents

P2 : Short-circuit current detection

P3: IGBT gate interrupt / Fault signal generation

P4: IGBT is slowly turned off

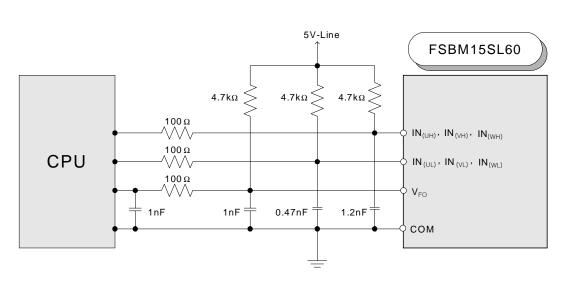
P5 : IGBT OFF signal

P6: IGBT ON signal - but IGBT cannot be turned on during the fault-output activation

P7 : IGBT OFF state

P8: Fault-output reset and normal operation start

Fig. 13. Short-circuit Current Protection (Low-side Operation only)



### Note:

It would be recommended that by-pass capacitors for the gating input signals, IN<sub>(XX)</sub> should be placed on the SPM pins and on the both sides of CPU and SPM for the fault output signal, V<sub>FO</sub>, as close as possible.

Fig. 14. Recommended CPU I/O Interface Circuit

These Values depend on PWM Control Algorithm

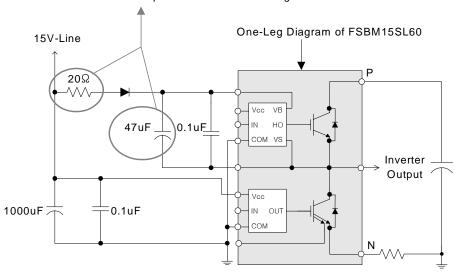
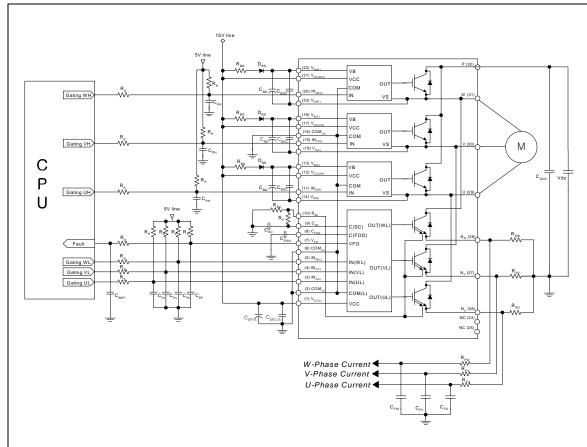


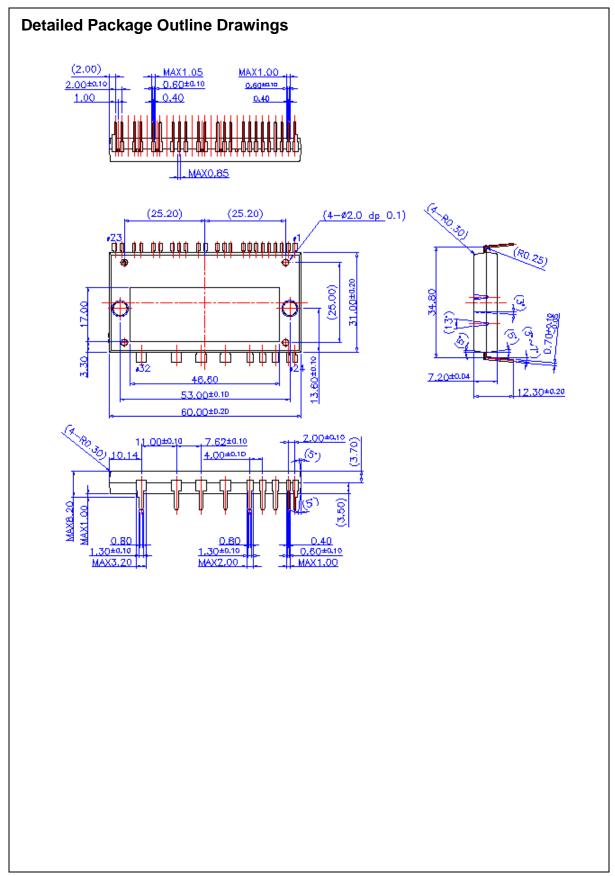
Fig. 15. Recommended Bootstrap Operation Circuit and Parameters



- 1. RpCpL/RpCpH coupling at each SPM input is recommended in order to prevent input signals' oscillation and it should be as close as possible to each SPM input pin.
- 2. By virtue of integrating an application specific type HVIC inside the SPM, direct coupling to CPU terminals without any opto-coupler or transformer isolation is possible.
- V<sub>FO</sub> output is open collector type. This signal line should be pulled up to the positive side of the 5V power supply with approximately 4.7kΩ resistance. Please refer to Fig. 16.
- $C_{\text{SP15}}$  of around 7 times larger than bootstrap capacitor  $C_{\text{BS}}$  is recommended.
- V<sub>FO</sub> output pulse width should be determined by connecting an external capacitor(C<sub>FOD</sub>) between C<sub>FOD</sub>(pin8) and COM<sub>(L)</sub>(pin2). (Example : if C<sub>FOD</sub> = 5.6 nF, then  $t_{FO} = 300 \,\mu s$  (typ.)) Please refer to the note 5 for calculation method.
- 6. Each input signal line should be pulled up to the 5V power supply with approximately 4.7kΩ resistance (other RC coupling circuits at each input may be needed depending on the PWM control scheme used and on the wiring impedance of the system's printed circuit board). Approximately a 0.22~2nF by-pass capacitor should be used across each power supply connection terminals.
- To prevent errors of the protection function, the wiring around R<sub>SC</sub>, R<sub>F</sub> and C<sub>SC</sub> should be as short as possible.
   In the short-circuit protection circuit, please select the R<sub>F</sub>C<sub>SC</sub> time constant in the range 3-4 μs. R<sub>F</sub> should be at least 30 times larger than R<sub>SC</sub>. (Recommended Example: R<sub>SC</sub> = 56 Ω, R<sub>F</sub> = 3.9kΩ, C<sub>SC</sub> = 1nF and R<sub>SU</sub> = R<sub>SV</sub> = 0Ω)
   For the use of shunt resistors (R<sub>SU</sub>, R<sub>SV</sub>, R<sub>SW</sub>), please see Fig. 7 in order to select the proper R<sub>SC</sub>.
   Each capacitor should be mounted as close to the pins of the SPM as possible.
- 11.To prevent surge destruction, the wiring between the smoothing capacitor and the P&N pins should be as short as possible. The use of a high frequency noninductive capacitor of around 0.1~0.22 uF between the P&N pins is recommended.
- 12. Relays are used at almost every systems of electrical equipments of home appliances. In these cases, there should be sufficient distance between the CPU and the relays. It is recommended that the distance be 5cm at least

Fig. 16. Application Circuit

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Rev. H5

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